



Fabrication of Nano-TiO₂ Coating for Dye-Sensitized Solar Cell by Vacuum Cold Spraying at Room Temperature

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Deposition of nanocrystalline TiO₂ coating at low temperature is becoming more attractive due to the possibility for continuous roll production of the coating for assembly lines of dye-sensitized solar cell (DSC) at a low cost. In this study, porous nano-TiO₂ coating was deposited by vacuum cold spraying (VCS) at room temperature on a conducting glass substrate using commercial P25 nanocrystalline TiO₂ powder. The microstructure of TiO₂ coating was characterized by field emission scanning electron microscopy (FESEM) and nitrogen adsorption test. A commercial dye (N719) was adsorbed on the surface of TiO₂ particles within the coating to assemble a DSC. The cell performance was evaluated by employing simulated solar light at an intensity of 100 mW/cm². The results showed that TiO₂ coating was deposited by the agglomerates of nano-TiO₂ powders. The Brunauer-Emmett-Teller (BET) test of the as-sprayed TiO₂ coating yielded a porosity of 49% and an average pore size of 17 nm. The assembled solar cell yielded a short-circuit current density of 7.3 mA/cm² and an energy conversion efficiency of 2.4%. The test results indicate that VCS was a promising method to deposit nanocrystalline TiO₂ coatings at low temperature applied to DSCs.

Keywords agglomerates, dye-sensitized solar cell, nanocrystalline material, porosity, TiO₂, vacuum cold spray

1. Introduction

At the beginning of 1990s, Grätzel and coworkers (Ref 1) reported a promising dye-sensitized solar cell (DSC) assembled using nanocrystalline TiO₂. High amounts of dye-molecules can be adsorbed due to large internal surface area of porous nanocrystalline coating. Consequently, the cells of a high light harvesting efficiency have been assembled. The solar power conversion efficiency of the cell reached a value higher than 11%,

which makes it a possible competitor of silicon solar cell because of its low cost (Ref 2). Nano-TiO₂ coating is usually prepared through at least two steps. At first step, TiO₂ is deposited on a conducting glass substrate using a suspension or a paste containing nano-TiO₂ particles in a desired size (Ref 3, 4). Organic binders, surfactants, and porosity controlling agents are usually added to the suspension to optimize the microstructure of the resulting nanocrystalline coating. In the second step, the sintering at a temperature of above 400 °C is commonly employed to promote the formation of a continuous nanoparticle network with sufficient cohesion, and electrical contact to the substrate and between the nanoparticles as well (Ref 5). The organic additives are burnt off during the sintering.

Transparent conducting oxide (TCO) coated glass is usually employed as substrate material of the DSC due to its excellent optical, electrical and encapsulation barrier properties, and compatibility with high-temperature processing. Recently, it is considered that flexible plastic substrates can be potentially used as the substrate for DSC. Using such substrates, roll-to-roll production techniques can be applied to cost-effective mass production of thin film solar cells (Ref 6). However, the usage of plastic substrates limits the selection of TiO₂ suspension and additives because polyethyleneterephthalate (PET) as a typical plastic substrate of DSC can only be processed at a temperature lower than 150 °C. Hence, with a plastic substrate, a simple suspension of TiO₂ nanoparticles in ethanol or water (Ref 6, 7) without any organic additive is required to deposit TiO₂ coatings. Due to the high surface tension of TiO₂ suspension without surfactants (Ref 8), it is difficult to form a uniform TiO₂ coating by conventional

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methods, including spin coating (Ref 9, 10), doctor blading (Ref 11, 12), and electrophoretical deposition (Ref 13, 14). The resultant TiO₂ coatings are generally crack-rich with a porosity of even as high as 80% (Ref 13).

Therefore, with plastic substrates, the low temperature processes were attempted to immobilize nanocrystalline TiO₂. The methods include low-temperature sintering (Ref 9, 12), hydrothermal crystallization (Ref 15, 16), chemical vapor deposition of Ti alkoxides (Ref 13), microwave irradiation (Ref 17, 18), UV light irradiation (Ref 13, 19), electron bombardment (Ref 20), and the room temperature compressing process (Ref 6, 21, 22). However, only a weak contact between TiO₂ particles is present in the TiO₂ coatings deposited by low temperature processes mentioned above. As a result, the assembled cell attained an energy conversion efficiency about half of the cells assembled using the TiO₂ coatings sintered at a high temperature (Ref 7, 14, 15). On the other hand, those reported results suggest that the nanocrystalline TiO₂ deposited by low temperature process can be applied to DSC.

Recently, a new spray deposition system, vacuum cold spraying (VCS), has been installed in our laboratory (Ref 23). In VCS, dry TiO₂ powder is directly deposited on a solid glass substrate to form a uniform coating under a reduced-pressure atmosphere at room temperature. TiO₂ coatings could be deposited through solid particle impact of high velocity achieved by high pressure gas. The high dynamic pressure on impact makes it possible to form TiO₂ coatings with "good" mechanical stability and contact between particles even without any post-treatment. Our previous study showed that the VCS TiO₂ coatings could be deposited using nano-TiO₂ powder to a thickness from several micrometers to several tens of micrometers through controlling deposition parameters.

In this study, TiO₂ coatings were deposited by VCS and employed to assemble DSC. For comparison, a cell was also assembled using the VCS TiO₂ coating post-sintered at 450 °C for 30 min in order to examine the contact condition between TiO₂ particles in the as-deposited coating through cell performance. F-doped tin oxide (FTO) conducting glass was used as a substrate. The microstructure of VCS TiO₂ coating was characterized by field emission scanning electron microscopy (FESEM) and nitrogen adsorption apparatus. The performance of the cells was investigated using a simulated solar light at an intensity of 100 mW/cm² generated by a 500 W Xe lamp.

2. Experimental

2.1 Materials

P25 (Degussa, Dusseldorf, Germany) TiO₂ powder was used as a feedstock for coating deposition by VCS. A transparent FTO conducting glass (TEC-15, LOF, Toledo, Ohio, USA) of 15 Ω/cm² was employed as a substrate with dimensions of 1.5 cm × 2 cm. The FTO substrate was cleaned, before spraying in an ultrasonic acetone bath. LiI with a purity of >98% (Lancaster Synthesis, Lancaster,

Table 1 Vacuum cold spraying parameters

Vacuum chamber pressure, Pa	2.3 × 10 ²
Pressure of the aerosol room, Pa	1 × 10 ⁶
He gas flow, L/min	2
Distance from nozzle exit to substrate, mm	5
Orifice size of nozzle, mm × mm	2.5 × 0.2
Substrate traverse speed, mm/s	5

UK), I₂ (A.R, Sanpu, Xi'an, China), and acetonitrile (G.R, Kermel, Tianjin, China) were used to prepare electrolyte. A commercially available dye-sensitizer (N719, Solaronix, Aubonne, Switzerland) was employed in this study.

2.2 Preparation of TiO₂ Coating

The TiO₂ coating was deposited using a home-developed VCS system (Ref 23). The system mainly constituted of a vacuum chamber, an accelerating gas feeding unit, a particle-accelerating nozzle, a two-dimensional worktable, and a control unit. The acceleration of TiO₂ particles was performed by high-pressure He gas. The coating thickness was about 15 μm. Spray parameters are given in Table 1.

2.3 Characterization of TiO₂ Powder and Coating

P25 TiO₂ powder consisted of agglomerates of primary nano-TiO₂ particles in a size of 25 nm in the diameter. The agglomerate size was measured by laser diffraction particle size analyzer (Mastersizer2000, Malvern Instruments Ltd., Malvern, UK). The topographic and cross-sectional morphologies of VCS TiO₂ coating were examined by FESEM (JSM-6700F, JEOL, Japan).

The porosity of VCS TiO₂ coating was estimated using a nitrogen adsorption-desorption apparatus (Coulter SA 3100 plus, Beckman Coulter, USA). The specific surface area was estimated by the Brunauer-Emmett-Teller (BET) equation and the pore size distribution was calculated by applying the Barret-Johner-Halenda (BJH) treatment to the desorption isotherm (Ref 24).

2.4 Fabrication of DSC

TiO₂ coating fabricated by VCS process was rinsed by absolute alcohol for anhydration. Then, it was soaked in a 3 × 10⁻⁴ mol L⁻¹ N719 dye solution of alcohol for 24 h at room temperature. A Pt counter electrode was prepared in a way given elsewhere (Ref 25). The counter electrode was placed on the top of the dye-coated TiO₂ coating and separated by a 40 μm thick tape (Zhengtai, Fujian, China) to assemble a sandwich-type solar cell. An electrolyte with 0.5 mol L⁻¹ LiI and 0.05 mol L⁻¹ I₂ in acetonitrile was employed.

2.5 Photoelectrochemical Measurement

The performance of the DSC was examined under the illumination of a Xe lamp (CHF-500 W, Chuangtuo, Beijing, China) with a RGB-3 filter for simulating solar light at an intensity of 100 mW/cm². The photocurrent-voltage curves were measured through using a 1000 Ω slide

reostat as a load in the outer circuit (Ref 26). The conversion efficiency (η) was characterized by the short-circuit photocurrent density (I_{SC}), the open-circuit voltage (V_{OC}), the fill factor of the cell (ff), and the intensity of the incident light ($I_s = 100 \text{ mW/cm}^2$) as follows:

$$\eta = I_{SC} \times V_{OC} \times ff / I_s \quad (\text{Eq 1})$$

3. Results and Discussion

3.1 Microstructure of TiO_2 Coating by VCS

Figure 1 shows the cross-sectional morphology of nanocrystalline TiO_2 coatings deposited by VCS using P25 TiO_2 powder. The coatings were deposited on the FTO glass substrates and then fractured. Figure 1a was the

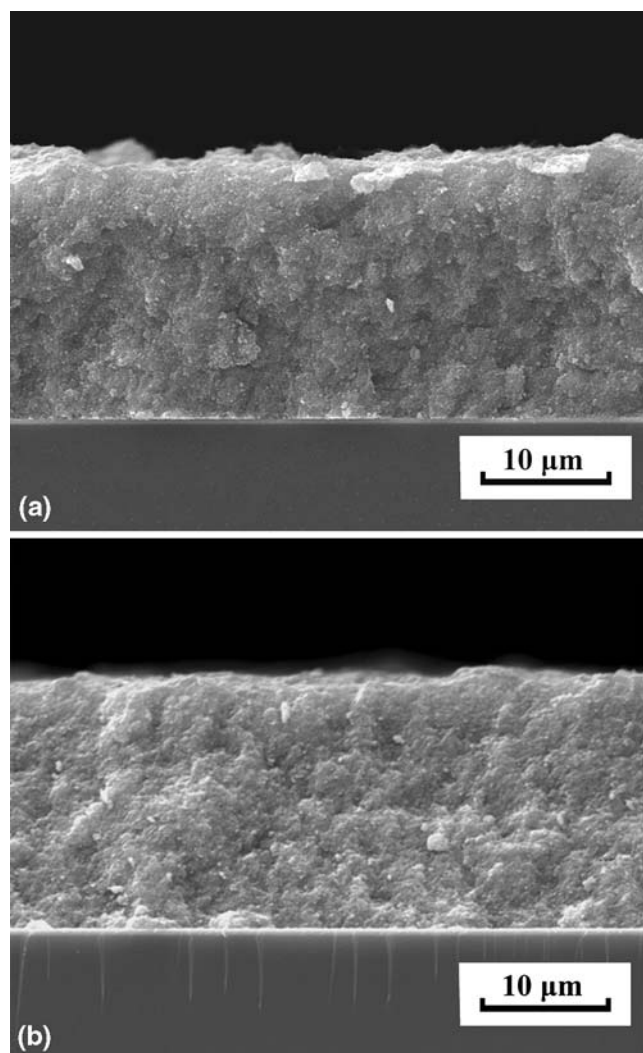


Fig. 1 Cross-sectional view of the nanocrystalline TiO_2 coating deposited on FTO glass substrate using P25 TiO_2 powders by vacuum cold spraying. (a) The as-sprayed TiO_2 coating, (b) the sintered TiO_2 coating at 450°C for 30 min

as-sprayed TiO_2 coating and Fig. 1b was the sintered one at 450°C for 30 min. It can be seen that the coatings were uniform in thickness. The thickness was $15 \mu\text{m}$.

P25 TiO_2 powder with a primary mean diameter of 25 nm was naturally agglomerated. The particle size distribution of agglomerates from the starting powders was characterized by laser diffraction particle analyzer (Fig. 2). Most agglomerated particles were in a size of several micrometers. Figure 3 shows typical surface morphology of TiO_2 coating prepared by the VCS process using P25 TiO_2 powder on the FTO substrate with the parameters shown in Table 1. It can be seen that TiO_2 coating was relatively compact in micrometer-sized scale, which was comparable with that deposited on ITO substrate (Ref 23). No obvious cracks were present in the

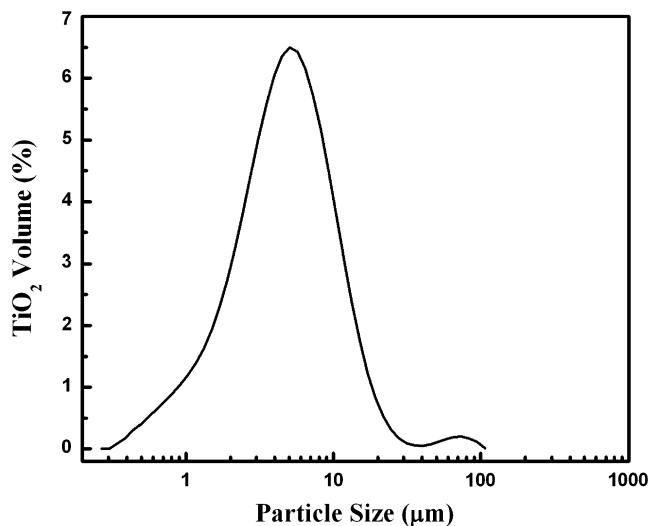


Fig. 2 Size distribution of agglomerates in P25 TiO_2 feedstock powder

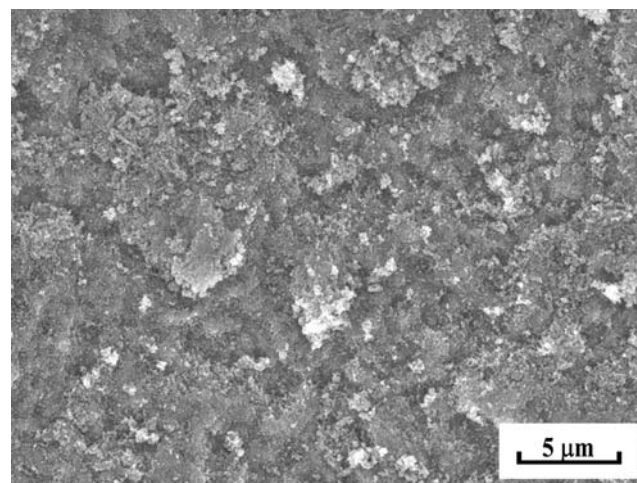


Fig. 3 Surface morphology of the nanocrystalline TiO_2 coating deposited on FTO glass substrate using P25 TiO_2 powders by vacuum cold spraying

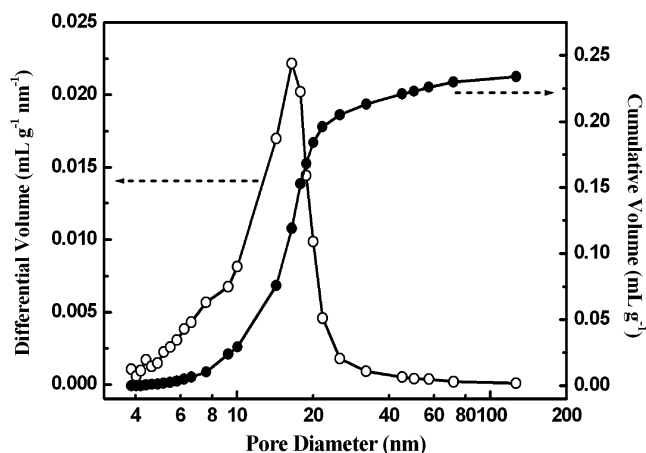


Fig. 4 Pore size distribution of TiO₂ coating deposited on FTO substrate by VCS using P25 TiO₂ powder

coating. Some large particles on the surface of the VCS TiO₂ coating have diameter of several micrometers comparable to that of TiO₂ agglomerates shown in Fig. 2. Therefore, possibly the deposition of TiO₂ nanocrystalline coating using P25 TiO₂ powder was achieved through the impact of the agglomerated particles. The compactness of the coating surface as shown in Fig. 3 implies that high contact pressure of impacting agglomerates at high velocity induced effectively the tamping effect on the deposited coating.

The pore size distribution of the VCS TiO₂ coating measured by the N₂ adsorption approach is presented in Fig. 4. The pore size ranged from 4 to 40 nm and the mean size was around 17 nm. The BET specific surface area was 56 m²/g, which was the same as that of the starting P25 TiO₂ powder. From the cumulative pore volume of about 0.24 cm³/g, the porosity of 49% was obtained, by taking 4.00 g/cm³ as the density of P25 TiO₂ (Ref 14).

3.2 Performance of DSC

Figure 5 shows photocurrent-voltage curve of a DSC assembled using the as-deposited TiO₂ coatings by VCS on the FTO conducting glass substrate. It can be seen that the test of the cell's performance yielded a short-circuit current density of 7.3 mA/cm², an open circuit voltage of 0.54 V and an overall conversion efficiency of 2.4%. These values are comparable to that of the cells assembled using TiO₂ coatings prepared by other methods at low temperature, such as mechanical compression (Ref 7) and hydrothermal crystallization (Ref 27). This fact indicates that vacuum cold spaying was an effective low-temperature deposition method for nanocrystalline TiO₂ coating applied to DSC.

It was considered that the contacts between TiO₂ agglomerates formed in a VCS TiO₂ coating resulted from mechanical impact of agglomerates. Such contacts are weak, which limits the improvement of cell performance. Generally, the contacts between nano-TiO₂ particles can be improved by a sintering treatment. In order to investigate the influence of particle contacts in the coating on DSC

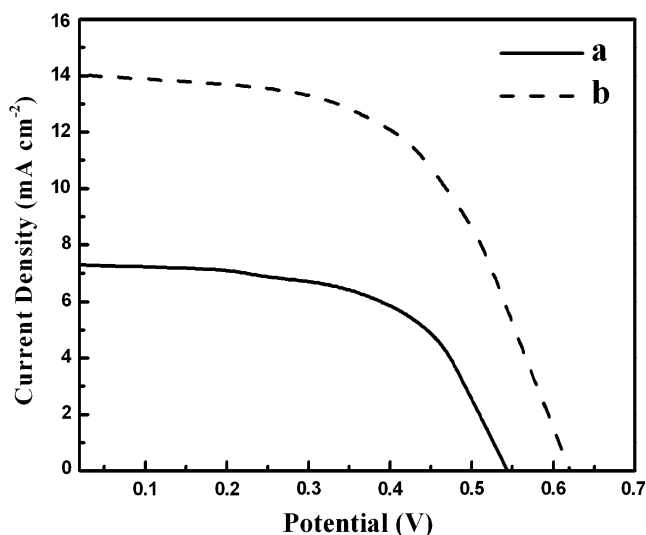
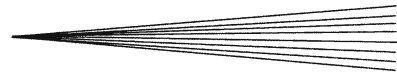


Fig. 5 Photocurrent-voltage characteristics of dye-sensitized solar cells composed of TiO₂ coating deposited by vacuum cold spraying on FTO substrate using P25 TiO₂ powder. (a) The cell assembled using the as-sprayed coating, (b) the cell assembled using the sintered coating at 450 °C for 30 min

cell's performance, a post-sintering at a temperature of 450 °C was applied to VCS TiO₂ coating for 30 min before assembly of solar cell. The performance of the cell composed of the annealed TiO₂ coating was shown in Fig. 5 for comparison. It is obvious that the short-circuit current density and conversion yield increased to 14.0 mA/cm² and 4.9%, respectively. Compared with the cell assembled using a sintered TiO₂ coating, the cell assembled with the as-sprayed TiO₂ coating reached about 50% of the short-circuit current density and the conversion yield. It was considered that the improvement of cell performance after sintering was attributed to the improvement of the contacts between nano-TiO₂ particles in the coating. On the other hand, this fact indicates that the contacts between nano-TiO₂ particles in the present coating attained only by impact were limited. Therefore, the improvement of cell performance should be attempted through improving the contacts between nano-TiO₂ particles in the as-sprayed coating by controlling deposition conditions.

4. Conclusions

TiO₂ coating was deposited by VCS at room temperature using 25 nm nano-TiO₂ feedstock powders. The porosity of the as-sprayed coatings estimated using N₂ adsorption method was 49% and the average pore size was 17 nm. The assembled solar cell yielded a short-circuit current density of 7.3 mA/cm² and an energy conversion efficiency of 2.4%. These results clearly indicated that VCS was a promising method to deposit nanocrystalline TiO₂ coatings at low temperature for DSC applications. Moreover, it was found that sintering the as-sprayed TiO₂ coating at a temperature of 450 °C for 30 min increased the short-current density and energy conversion efficiency



of the cell by a factor of 2. This result clearly suggests that the contact between nano-TiO₂ particles in the nanocrystalline deposit significantly influences the cell's performance. It can be considered that the controlling of particle contact through deposition conditions benefits the improvement of DSC performance.

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